

## PATENT ABSTRACTS OF JAPAN

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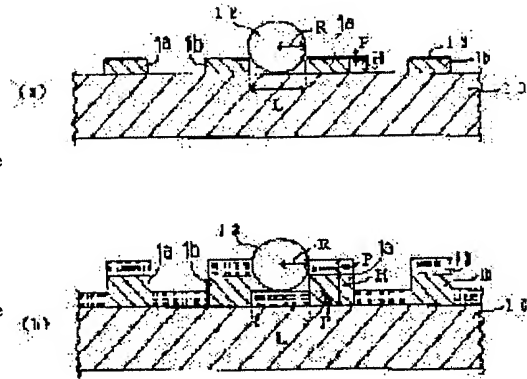
(21)Application number : 08-258154 (71)Applicant : KYOCERA CORP  
 (22)Date of filing : 30.09.1996 (72)Inventor : MATSUDA TOSHIYA  
 OTSUKA KAZUHIRO  
 IIOKA ATSUHIRO  
 KAGAI EMI  
 KISHU ATSUO

## (54) SURFACE ACOUSTIC WAVE DEVICE

## (57)Abstract:

**PROBLEM TO BE SOLVED:** To manufacture a surface acoustic wave(SAW) device at a low cost with a simple process in which a short-circuit between electrode fingers due to deposition of a conductive foreign material is suppressed.

**SOLUTION:** A photosensing resist for lift-off is coated on a piezoelectric substrate 10 made of a 36° Y-cut - X propagation LiTaO<sub>3</sub> crystal, a negative pattern of an interdigital transducer(IDT) electrode is formed and the width of electrode fingers 1a, 1b is selected to 1.1μm, and the interval between the electrode fingers 1a, 1b is selected to 1.1μm. Then an aluminum film is formed on the surface of the piezoelectric substrate on which the negative pattern is in existence by the thickness of 460nm by the vacuum vapor-deposition method and a silicon film for a protection film 13 is formed 35nm thick without breaking the vacuum state. The photosensing resist, the conductor film and the protection film 13 equivalent to the negative pattern of the piezoelectric substrate 10 are lifted off to manufacture the SAW device. The film thickness of the IDT electrodes of the SAW device is selected to 460nm and a half of the interval between the electrode fingers 1a and 1b of the SAW device is selected to 550nm.



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## CLAIMS

[Claim(s)]

[Claim 1] Surface acoustic wave equipment which arranges so that the electrode finger of the both sides of the ctenidium-like electrode of a pair which have two or more parallel electrode fingers on a piezo-electric substrate may gear mutually, and is surface acoustic wave equipment which prepares a protective coat only on a these ctenidium-like electrode, and changes, and is characterized by carrying out to less than [ of spacing between the electrode fingers which adjoin the thickness of said ctenidium-like electrode ] 1/2.

[Claim 2] The surface acoustic wave equipment which arranges so that the electrode finger of the both sides of the ctenidium-like electrode of a pair which have two or more parallel electrode fingers on a piezo-electric substrate may gear mutually, and is surface acoustic wave equipment which prepares a protective coat on a these ctenidium-like electrode and a piezo-electric substrate front face, and changes, and is characterized by to make the difference of the thickness of said ctenidium-like electrode, and the thickness of a protective coat less than [ of spacing between adjoining electrode fingers ] into 1/2.

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## DETAILED DESCRIPTION

## [Detailed Description of the Invention]

[0001]

[Field of the Invention] This invention is surface acoustic wave equipment for a resonator and frequency band filters built in mobile wireless devices, such as a land mobile radiotelephone and a cellular phone, and relates to the surface acoustic wave equipment considered as the configuration in which the electrode formed on the piezo-electric substrate controls the short-circuit by adhesion of a conductive foreign matter.

[0002]

[Description of the Prior Art] Conventional surface acoustic wave (it omits Surface Acoustic Wave and Following SAW) equipment is shown in drawing 2, and the production process is shown in drawing 4. Although (a) of drawing 2 prepared the partial expanded sectional view of SAW equipment and (b) prepared the protective coat, a partial expanded sectional view and (c) are the top views of the basic configuration of the whole equipment.

[0003] It sets to (a) of this drawing, and is LiNbO<sub>3</sub>. A crystal and LiTaO<sub>3</sub> On the piezo-electric substrates 10, such as a crystal, the IDT (Inter Digital Transducer) electrode 11 of the ctenidium-like electrode arranged so that the predetermined spacing L may be set and two or more parallel electrode fingers 11a and 11b of each other may be clenched is formed. (b) is the configuration of having formed the insulating or semi-conductive protective coat 13 in the whole surface of the substrate side in which the IDT electrode 11 was formed, in order to hold the insulation between electrode finger 11a and 11b, when the conductive particle 12 adheres between electrode finger 11a and 11b [ electrode finger 11a and 11b top or ].

[0004] In (c) of this drawing, 11a was the electrode finger of an input side, 11b was the electrode finger of an output side, and when between electrode finger 11a and 11b flowed and short-circuited, the property as a resonator or a frequency band filter (henceforth a filter) had deteriorated. in addition -- general -- an IDT electrode -- a logarithm -- several 10 -- a number -- although it was about 100, in (c), it drew typically.

[0005] Such SAW equipment is manufactured at a process as shown in drawing 4. The photosensitive resist for lift off is applied on the piezo-electric substrate 10 at a process (a), and the negative pattern of the IDT electrode 11 is formed by the photolithography method at a process (b). After an appropriate time, at a process (c), the electric conduction film for IDT electrode 11 which consists of a metal or an alloy is formed in a vacuum ambient atmosphere by the thin film forming methods, such as vacuum deposition and the sputtering method, the piezo-electric substrate 10 is taken out out of a vacuum ambient atmosphere at a process (d), the photosensitive resist and electric conduction film of the negative pattern section are removed by the lift-off method (or the etching method), and the IDT electrode 11 of a request pattern is formed. And a protective coat 13 is made to form by vacuum deposition, the sputtering method, etc. on the IDT electrode 11 at a process (e). At this time, the piezo-electric substrate 10 was put in into the vacuum ambient atmosphere at 2 times of processes, (c) and (e).

[0006]

[Problem(s) to be Solved by the Invention] however -- if the protective coat 13 is not formed on the IDT electrode 11 -- abbreviation -- when the spherical conductive particle 12 adhered, there was a problem of between electrode finger 11a and 11b having flowed [ the radius R ] at the time of  $R > L/2$  (L being the distance between electrode finger 11a and 11b), and short-circuiting. Moreover, since a protective coat 13 cannot disregard the effect which it has on a resonator property or a filter shape even if it is going to form a protective coat 13 all over the substrate side in which the IDT electrode 11 was formed and is going to hold the insulation between electrode finger 11a and 11b. For example, thickness of a protective coat 13 had to be made thin as thickness of a protective coat 13 was set to about 50nm to about 500nm of thickness of the IDT electrode 11. Therefore, when the covering nature of a protective coat 13 was inadequate, and a protective coat 13 was not fully formed in the side face of the electrode fingers 11a and 11b, therefore  $R = L / \text{about two particle 12 fitted in between electrode finger 11a and 11b}$  exactly, it short-circuited through the side face of the electrode fingers 11a and 11b.

[0007] Moreover, when making a protective coat 13 form on the IDT electrode 11 by the thin film forming method for using vacuum devices, such as vacuum deposition and the sputtering method, the piezo-electric substrate 10 is again put in into the vacuum ambient atmosphere, and, for this reason, vacuum suction of vacuum devices needed to be performed twice [ at least ]. Furthermore, while taking the piezo-electric substrate 10 in and out out of the vacuum ambient atmosphere, the foreign matter might adhere on the piezo-electric substrate 10 or the IDT electrode 11.

[0008] Therefore, this invention is completed in view of the above-mentioned situation, the purpose controls the short-circuit between the electrode fingers by adhesion of a conductive foreign matter, and it is in manufacturing the SAW equipment of such a configuration to low cost at a simple process.

[0009]

[Means for Solving the Problem] The surface acoustic wave equipment of the 1st invention is arranged so that the electrode finger of the both sides of the ctenidium-like electrode of a pair which have two or more parallel electrode fingers on a piezo-electric substrate may gear mutually, and it is characterized by to carry out to less than [ of spacing between the electrode fingers which are surface acoustic wave equipment which prepares a protective coat only on a these ctenidium-like electrode, and changes, and adjoin the thickness of said ctenidium-like electrode ]  $1/2$ .

[0010] The surface acoustic wave equipment of the 2nd invention is arranged so that the electrode finger of the both sides of the ctenidium-like electrode of a pair which have two or more parallel electrode fingers on a piezo-electric substrate may gear mutually. And it is surface acoustic wave equipment which prepares a protective coat in a these ctenidium-like electrode and a piezo-electric substrate front face, and grows into them, and is characterized by making the difference of the thickness of said

ctenidium-like electrode, and the thickness of a protective coat less than [ of spacing between adjoining electrode fingers ] into 1/2.

[0011]

[Embodiment of the Invention] Drawing 1 explains a production process for the surface acoustic wave equipment of this invention using drawing 3. It is the partial expanded sectional view of SAW equipment [ in / (a) of drawing 1, and / in (b) / other operation gestalten ]. [ the partial expanded sectional view of SAW equipment ] For a piezo-electric substrate and H, the thickness of an IDT electrode and L are [ two or more parallel electrode fingers of the IDT electrode which is a ctenidium-like electrode of the pair arranged by (a) of this drawing, and (b) so that 1a and 1b may be clenched mutually, and 10 / the thickness of a protective coat 13 and R of spacing between electrode finger 1a and 1b and P ] the radii of the conductive particle 12. (a) - (e) of drawing 3 explains the contents of each process briefly. In addition, in drawing 1, the same sign is given to the same member as drawing 2.

[0012] In  $2R < L$ , in (a) of drawing 1, the electrode fingers 1a and 1b of the both sides of the ctenidium-like electrode of a pair do not short-circuit. In  $2R > L$ , a particle 12 adheres over two or more electrode fingers top, but since the protective coat 13 is formed on the IDT electrode (only on an IDT electrode), it does not short-circuit. Although a particle 12 may contact and short-circuit on the side face of the electrode fingers 1a and 1b in  $2R \approx L$ , with this operation gestalt, it is referred to as  $H < L/2$ , and the side face of the electrode fingers 1a and 1b has not reached the part of the maximum width of a particle 12. therefore, the probability which short-circuits through the side face of the electrode fingers 1a and 1b is markedly alike, and becomes small.

[0013] In  $2R < L$  and  $2R > L$ , in (b) of drawing 1, it does not short-circuit like (a). Like  $H > L/2$ , this operation gestalt is applied, when the thickness of an IDT electrode is comparatively thick, and the side face of the electrode fingers 1a and 1b has not reached the part of the maximum width of a particle 12 by setting to  $H - P < L/2$  height H-P of the side face of the electrode fingers 1a and 1b exposed outside. therefore, the probability which short-circuits through the side face of the electrode fingers 1a and 1b is markedly alike, and becomes small.

[0014] For the above-mentioned protective coat 13,  $\rho/P$  is 109, when it consists of an insulating or semi-conductive (half-conductivity) thing electrically and the resistivity of a protective coat is set to  $\rho$  (ohm-cm). It is desirable to make it become the above ( $\omega$ ). As the ingredient, they are Ta, Mo and those oxides or a nitride, NiCr, NiCr-Si, Cr-SiO, Cr-SiO<sub>2</sub>, Si, SiO<sub>2</sub>, SiN, etc.

[0015] In this invention, it consists of aluminum or an aluminum alloy (an aluminum-Cu system, aluminum-Ti system, etc.), and especially aluminum has high excitation effectiveness, an IDT electrode has cheap ingredient cost and it is desirable. Moreover, although an electrode configuration is a configuration which engaged the ctenidium-like electrode for I/O (IDT electrode) as shown in drawing 1 by turns, this invention can apply two or more electrode fingers also to the thing of a slit mold like the reflector arranged in parallel. Furthermore, the cross-section configuration of the electrode fingers 1a and 1b is desirable when an inverse tapered shape mold which is tapering off toward a piezo-electric substrate side controls short-circuiting through the side face of the electrode fingers 1a and 1b.

[0016] The logarithm of an IDT electrode the width of face of 50 to about 200, and the electrode fingers 1a and 1b And about 0.1-10.0 micrometers, The crossover width of face of about 0.1-10.0 micrometers and the electrode fingers 1a and 1b is suitable for spacing between electrode finger 1a and 1b, when setting thickness of about 10-80 micrometers and an IDT electrode to about 0.2-0.4 micrometers acquires the expected property as a resonator or a filter. Moreover, if the reflector for reflecting SAW in the both ends of the propagation path of SAW of an IDT electrode, and resonating them efficiently may be prepared suitably and piezoelectric material, such as ZnO and AlO, is further formed between electrode finger 1a and 1b, the resonance effectiveness of SAW improves and is suitable.

[0017] As the above-mentioned piezo-electric substrate 10, it is LiTaO<sub>3</sub> of 36 degreeY cut-X propagation, Crystal, LiNbO<sub>3</sub> of 64 degreeY cut-X propagation LiB 407 of a crystal and 45-degreeX cut-Z propagation Crystal, Xtal etc. is suitable and it is LiTaO<sub>3</sub> of 36 degreeY cut-X propagation especially. Pass band width is wide and a crystal is LiB 407 of 45-degreeX cut-Z propagation. Since [ that an electromechanical coupling coefficient is large and ] the group delay temperature coefficient of a crystal is small, it is desirable. The thickness of the piezo-electric substrate 10 has 0.3-0.5 goodmm, the piezo-electric substrate 10 becomes weak in less than 0.3mm, and cost becomes large in 0.5mm \*\*.

[0018] in this way, this invention has the operation effectiveness of boiling markedly the short-circuit between the electrode fingers by adhesion of a conductive foreign matter, and controlling it.

[0019] Furthermore, the SAW equipment of this invention is manufactured as follows. In (a) of drawing 1, the process of drawing 3 is followed. First, the photosensitive resist for lift off is applied on the piezo-electric substrate 10 at a process (a), and the negative pattern of an IDT electrode is formed by the photolithography method at a process (b). Then, the electric conduction film which consists of aluminum for IDT electrodes etc. in a vacuum ambient atmosphere is formed at a process (c) by the thin film forming methods, such as vacuum deposition, the sputtering method, and a CVD method. It is made for the thickness of the electric conduction film to become less than [ of spacing between electrode finger 1a and 1b ] 1/2 then. Next, a protective coat 13 is formed with vacuum deposition etc. on the near piezo-electric substrate front face in which the IDT electrode was formed, without breaking a vacuum at a process (d). 10-100nm is suitable for the thickness, and less than 10nm is not enough for it to function as an insulating protective coat 13, and it has big effect on a resonator property and a filter shape in 100nm \*\*. And lift off of the photosensitive resist which is equivalent to the negative pattern section at a process (e), the electric conduction film, and the protective coat 13 is carried out to coincidence, and the SAW equipment of this invention is obtained.

[0020] In (b) of drawing 1, the following processes are followed. First, on the piezo-electric substrate 10, the photosensitive resist for lift off is applied and the negative pattern of an IDT electrode is formed by the photolithography method. Then, the electric conduction film for IDT electrodes which consists of aluminum etc. is formed by the thin film forming methods, such as vacuum deposition, the sputtering method, and a CVD method. With a photosensitive resist, lift off of the electric conduction film equivalent to a negative pattern is carried out, it is removed, and an IDT electrode is formed. In addition, after an IDT electrode forms the electric conduction film first, applies a photosensitive resist and forms the positive pattern of an IDT electrode by the photolithography method, it may leave and form the electric conduction film equivalent to a positive pattern by the etching method.

[0021] Next, a protective coat is formed by the thin film forming methods, such as vacuum deposition, the sputtering method, and a CVD method. 10-100nm is suitable for the thickness like the case of (a) of drawing 1. At this time, it is made for the difference of the thickness of an IDT electrode and the thickness of a protective coat 13 to become less than [ of spacing between electrode finger 1a and 1b ] 1/2, and the surface acoustic wave equipment of this invention is obtained.

[0022] In addition, this invention is not limited to the above-mentioned operation gestalt, and modification various by within the

limits which does not deviate from the summary of this invention does not interfere at all.

[0023]

[Example] The example of this invention is shown below.

[0024] (Example 1) It is the following, and the SAW equipment equivalent to (a) of drawing 1 was made and produced. LiTaO<sub>3</sub> of 36 degreeY cut-X propagation On the piezo-electric substrate 10 which consists of a crystal, the photosensitive resist for lift off was applied and the negative pattern of an IDT electrode was formed by the photolithography method. At this time, conditions, such as the baking temperature of a photosensitive resist, BEKU time amount, ultraviolet-rays reinforcement at the time of exposure, the exposure time, a developer, and developing time, were adjusted, and that cross-section configuration was made into the inverse tapered shape configuration so that it might be easy to carry out lift off of the photosensitive resist. It is SAW LiTaO<sub>3</sub> Since X shaft orientations of a crystal were made to spread, it was made for the longitudinal direction of the electrode fingers 1a and 1b to become perpendicular to X shaft orientations. Moreover, since about 900MHz signal is passed, in order to acquire a desired property, it was made for spacing whose width of face of the electrode fingers 1a and 1b is between 1.1 micrometers, electrode finger 1a, and 1b to be set to 1.1 micrometers.

[0025] Next, the piezo-electric substrate 10 was installed in the vacuum deposition inside of a plane, and 460nm of aluminum was formed on the near piezo-electric substrate front face in which the negative pattern was formed. At this time, the degree of vacuum in the chamber of a vacuum deposition machine was set to 10-7Torr. Then, 25nm of Si for protective coat 13 was formed, without breaking a vacuum. At this time, discharge took place between electrode finger 1a and 1b according to the pyroelectric effect of the piezo-electric substrate 10, and in order to avoid that the electrode fingers 1a and 1b are damaged, heating of the piezo-electric substrate 10 was not performed. And lift off of the photosensitive resist equivalent to the negative pattern of the piezo-electric substrate 10, the electric conduction film, and the protective coat 13 was carried out, the IDT electrode and the protective coat 13 were formed, and SAW equipment was produced.

[0026] The above-mentioned SAW equipment = (thickness of an IDT electrode) it was 460nm and, on the other hand, was  $= (1/2 \text{ of spacing between electrode finger 1a and 1b}) \cdot 1.1 \text{ (micrometer)} / 2 = 550 \text{ (nm)}$ . By considering as said configuration, that whose percent defective was several % conventionally decreased to about 0.1%. Moreover, since vacuum suction was managed at once as compared with the former, the part SAW equipment has been manufactured to low cost.

[0027] (Example 2) It is the following, and the SAW equipment equivalent to (b) of drawing 1 was made and produced. LiTaO<sub>3</sub> of 36 degreeY cut-X propagation On the piezo-electric substrate 10 which consists of a crystal, the photosensitive resist for lift off was applied and the negative pattern of an IDT electrode was formed by the photolithography method. At this time, conditions, such as the baking temperature of a photosensitive resist, BEKU time amount, ultraviolet-rays reinforcement at the time of exposure, the exposure time, a developer, and developing time, were adjusted, and that cross-section configuration was made into the inverse tapered shape configuration so that it might be easy to carry out lift off. It is SAW LiTaO<sub>3</sub> Since X shaft orientations of a crystal were made to spread, it was made for the longitudinal direction of the electrode fingers 1a and 1b to become perpendicular to X shaft orientations. Moreover, since about 900MHz signal is passed, in order to acquire a desired property, it was made for spacing whose width of face of the electrode fingers 1a and 1b is between 1.1 micrometers, electrode finger 1a, and 1b to be set to 1.1 micrometers.

[0028] Next, the piezo-electric substrate 10 was installed in the vacuum deposition inside of a plane, and 460nm of aluminum was formed on the near piezo-electric substrate front face in which the negative pattern was formed. At this time, the degree of vacuum in the chamber of a vacuum deposition machine was set to 10-7Torr. Lift off of the photosensitive resist equivalent to the negative pattern of the piezo-electric substrate 10 after vacuum evaporatio~~no~~ was carried out, and the IDT electrode was formed. Then, the piezo-electric substrate 10 was installed in the vacuum deposition inside of a plane, vacuum suction was carried out to the 10-7Torr base, 25nm of Si for protective coat 13 was formed, and SAW equipment was produced. At this time, discharge took place between electrode fingers according to the pyroelectric effect of the piezo-electric substrate 10, and in order to avoid that an electrode finger is damaged, heating of the piezo-electric substrate 10 was not performed.

[0029] The above-mentioned SAW equipment is (thickness of IDT electrode)-(thickness of protective coat 13) =  $460 - 25 = 435 \text{ (nm)}$ . On the other hand, since it is  $= (1/2 \text{ of spacing between electrode finger 1a and 1b}) \cdot 1.1 \text{ (micrometer)} / 2 = 550 \text{ (nm)}$ , 435nm of differences of the thickness of an IDT electrode and the thickness of a protective coat 13 serves as one half of values of spacing between electrode finger 1a and 1b smaller than 550nm. By making it said configuration, the same effectiveness as an example 1 was acquired.

[0030]

[Effect of the Invention] a protective coat is prepared only on a ctenidium-like electrode and invention of the 1st of this invention does so the effectiveness that it boils markedly that a conductive foreign matter adheres at the time of assembly processing of packaging etc., and short-circuit occurs between electrode fingers, and can control, by making thickness of a ctenidium-like electrode less than [ of spacing between electrode fingers ] into 1/2. Moreover, since a ctenidium-like electrode and a protective coat can be formed continuously, without breaking a vacuum and a photolithography process can also be managed at once, a process is simplified. Furthermore, when releasing a vacuum, contamination of a foreign matter mixing and adhering into an ambient atmosphere from the exterior decreases. Since a protective coat is formed before finishing forming a ctenidium-like electrode, there is no discharge between the electrode fingers by the pyroelectric effect at the time of protective coat formation, and it also has the effectiveness that an electrode finger is not damaged.

[0031] moreover, a protective coat is prepared in a ctenidium-like electrode and a piezo-electric substrate front face, and by making the difference of the thickness of a ctenidium-like electrode, and the thickness of a protective coat less than [ of spacing between electrode fingers ] into 1/2, like the above, the 2nd invention boils markedly that short-circuit occurs, and can be controlled between electrode fingers. In this case, when it is not necessary to cover a protective coat on the side face of an electrode finger or and a protective coat is not covered with a certain cause by the side face of an electrode finger, short-circuit can be controlled if the thickness of a ctenidium-like electrode is adjusted like this invention. Therefore, since membranes can be formed also by the bad membrane formation equipment of covering nature, and the membrane formation approach, it is not restrained by membrane formation facility but manufacture becomes possible by low cost. Since covering of the side face of an electrode finger which membrane formation cannot carry out easily is not needed, thickness of a protective coat can be made thin, the tact time of membrane formation becomes short, and productivity is good. Moreover, effect on a resonator property and an SAW filter property can be made small by thin film-ization of a protective coat, therefore the degree of freedom of a design improves.

[0032] Furthermore, since the probability of this invention which short-circuits even if a conductive foreign matter adheres to some extent is quite small, it becomes unnecessary to wash too much the package which are the main generation sources of a

conductive foreign matter consequently, and it can simplify a production process.

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## DESCRIPTION OF DRAWINGS

## [Brief Description of the Drawings]

[Drawing 1] Although the SAW equipment of this invention is shown and (a) has a protective coat only on an IDT electrode, although a partial expanded sectional view and (b) have a protective coat in the whole surface, they are a partial expanded sectional view.

[Drawing 2] Although conventional SAW equipment is shown and (a) does not have a protective coat, although a partial expanded sectional view and (b) have a protective coat in the whole surface, they are a partial expanded sectional view.

[Drawing 3] In the flow chart of the production process of the SAW equipment of this invention, (a) - (e) shows the contents of each process.

[Drawing 4] In the flow chart of the production process of conventional SAW equipment, (a) - (e) shows the contents of each process.

## [Description of Notations]

- 1a: Electrode finger
- 1b: Electrode finger
- 10: A piezo-electric substrate
- 12: A conductive particle
- 13: Protective coat

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(71) 出願人 000006633

京セラ株式会社

京都府京都市山科区東野北井ノ上町5番地の22

(72) 発明者 松田 敏哉

京都府相楽郡精華町光台3丁目5番地 京セラ株式会社中央研究所内

(72) 発明者 大塚 一弘

京都府相楽郡精華町光台3丁目5番地 京セラ株式会社中央研究所内

(72) 発明者 飯岡 淳弘

京都府相楽郡精華町光台3丁目5番地 京セラ株式会社中央研究所内

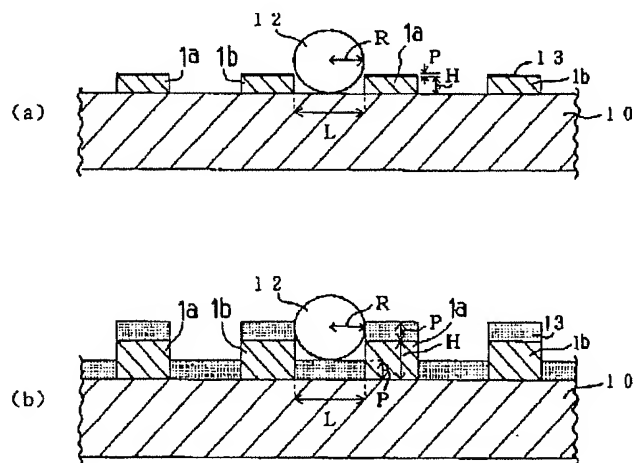
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(54) 【発明の名称】 弾性表面波装置

(57) 【要約】

【課題】導電性の異物の付着による電極指間のショートを抑制し、SAW装置を簡略な工程で低コストに製造する。

【解決手段】 $36^\circ$  Yカット-X伝搬のLiTaO<sub>3</sub>結晶から成る圧電基板10上にリフトオフ用の感光性レジストを塗布し、フォトリソグラフィ法によりIDT電極のネガパターンを形成し、電極指1a, 1bの幅は $1.1\mu\text{m}$ 、電極指1a, 1b間の間隔は $1.1\mu\text{m}$ とした。次に、真空蒸着法によりネガパターンのある側の圧電基板表面にAlを460nm成膜し、真空を破らずに保護膜13用のSiを35nm成膜した。圧電基板10のネガパターンに相当する感光性レジスト、導電膜、保護膜13をリフトオフし、SAW装置を作製した。SAW装置は(IDT電極の膜厚) $=460\text{nm}$ で、(電極指1a, 1b間の間隔の $1/2$ ) $=550\text{nm}$ であった。





## 【特許請求の範囲】

【請求項1】圧電基板上に、複数の平行な電極指を有する一対の櫛歯状電極の双方の電極指が互いに噛み合うように配置し、かつこれら櫛歯状電極上のみに保護膜を設けて成る弾性表面波装置であって、前記櫛歯状電極の厚さを隣接する電極指間の間隔の $1/2$ 未満としたことを特徴とする弾性表面波装置。

【請求項2】圧電基板上に、複数の平行な電極指を有する一対の櫛歯状電極の双方の電極指が互いに噛み合うように配置し、かつこれら櫛歯状電極及び圧電基板表面に保護膜を設けて成る弾性表面波装置であって、前記櫛歯状電極の厚さと保護膜の膜厚との差を、隣接する電極指間の間隔の $1/2$ 未満としたことを特徴とする弾性表面波装置。

## 【発明の詳細な説明】

## 【0001】

【発明の属する技術分野】本発明は、自動車電話及び携帯電話等の移動体無線機器に内蔵される共振器及び周波数帯域フィルタ用の弾性表面波装置であって、圧電基板上に形成された電極が、導電性の異物の付着によるショ

## 【0002】

【従来の技術】従来の弾性表面波（Surface Acoustic Wave、以下SAWと略す）装置を図2に、その製造工程を図4に示す。図2の（a）はSAW装置の部分拡大断面図、（b）は保護膜を設けたものの部分拡大断面図、（c）は装置全体の基本構成の平面図である。

【0003】同図の（a）において、 $\text{LiNbO}_3$ 結晶、 $\text{LiTaO}_3$ 結晶等の圧電基板10上に、所定の間隔 $L$ において複数の平行な電極指11a、11bが互いに噛み合わされるように配置された、櫛歯状電極のIDT（Inter Digital Transducer）電極11が設けられている。（b）は、電極指11a、11b上若しくは電極指11a、11b間に導電性の微粒子12が付着した場合に、電極指11a、11b間の絶縁性を保持するために、IDT電極11が設けられた基板面の全面に絶縁性又は半導電性の保護膜13を設けた構成である。

【0004】同図の（c）において、11aは例えば入力側の電極指で、11bは例えば出力側の電極指であり、電極指11aと11b間が導通しショートすると、共振器や周波数帯域フィルタ（以下フィルタという）としての特性が劣化していた。尚、一般的に、IDT電極対数は数10～数100程度であるが、（c）では模式的に描いた。

【0005】このようなSAW装置は、図4に示すような工程で製造される。工程（a）で圧電基板10上にリフトオフ用の感光性レジストを塗布し、工程（b）でフォトリソグラフィー法によりIDT電極11のネガパターンを形成する。しかる後、工程（c）で蒸着法やスパッタリング法等の薄膜形成法により、金属又は合金から

成るIDT電極11用の導電膜を真空雰囲気中で成膜し、工程（d）で圧電基板10を真空雰囲気中から取り出し、リフトオフ法（またはエッチング法）によりネガパターン部の感光性レジストと導電膜を除去し、所望パターンのIDT電極11を形成する。そして、工程（e）でIDT電極11上に蒸着法やスパッタリング法等で保護膜13を形成させる。このとき、（c）と（e）の2回の工程で、圧電基板10を真空雰囲気中に入れていた。

## 【0006】

【発明が解決しようとする課題】しかしながら、IDT電極11上に保護膜13が設けられていないと、略球状の導電性の微粒子12が付着した場合、その半径 $R$ が $R \geq L/2$ （ $L$ は電極指11a、11b間の間隔）のとき、電極指11a、11b間が導通しショートするという問題があった。また、IDT電極11が設けられた基板面の全面に保護膜13を設けて、電極指11a、11b間の絶縁を保持しようとしても、保護膜13が共振器特性やフィルタ特性に与える影響が無視できないため、例えばIDT電極11の膜厚500nm程度に対して保護膜13の膜厚を50nm程度にするというように、保護膜13の膜厚を薄くせざるをえなかった。そのため保護膜13の被覆性が不十分で、電極指11a、11bの側面には保護膜13が十分に形成されず、従って、ちょうど $R = L/2$ 程度の微粒子12が電極指11a、11b間に嵌まり込んだ場合に、電極指11a、11bの側面を通じてショートしていた。

【0007】また、IDT電極11上に蒸着法やスパッタリング法等の真空装置を利用する薄膜形成法で保護膜13を形成させる場合に、圧電基板10を再度真空雰囲気中に入れており、このため、真空装置の真空引きを最低2度行う必要があった。更に、圧電基板10を真空雰囲気中に出し入れする間に、圧電基板10やIDT電極11上に異物が付着することがあった。

【0008】従って、本発明は上記事情に鑑みて完成されたものであり、その目的は導電性の異物の付着による電極指間のショートを抑制し、そのような構成のSAW装置を簡略な工程で低コストに製造することにある。

## 【0009】

【課題を解決するための手段】第1の発明の弾性表面波装置は、圧電基板上に、複数の平行な電極指を有する一対の櫛歯状電極の双方の電極指が互いに噛み合うように配置し、かつこれら櫛歯状電極上のみに保護膜を設けて成る弾性表面波装置であって、前記櫛歯状電極の厚さを隣接する電極指間の間隔の $1/2$ 未満としたことを特徴とする。

【0010】第2の発明の弾性表面波装置は、圧電基板上に、複数の平行な電極指を有する一対の櫛歯状電極の双方の電極指が互いに噛み合うように配置し、かつこれら櫛歯状電極及び圧電基板表面に保護膜を設けて成る弾

性表面波装置であって、前記櫛歯状電極の厚さと保護膜の膜厚との差を、隣接する電極指間の間隔の $1/2$ 未満としたことを特徴とする。

#### 【0011】

【発明の実施の形態】本発明の弾性表面波装置を図1で、製造工程を図3を用いて説明する。図1の(a)はSAW装置の部分拡大断面図、(b)は他の実施形態におけるSAW装置の部分拡大断面図である。同図の

(a), (b)で、1a, 1bは、互いに噛み合わされるように配置された一対の櫛歯状電極であるIDT電極の複数の平行な電極指、10は圧電基板、HはIDT電極の膜厚、Lは電極指1a, 1b間の間隔、Pは保護膜13の膜厚、Rは導電性の微粒子12の半径である。図3の(a)~(e)は各工程の内容を簡単に説明したものである。尚、図1において、図2と同じ部材には同じ符号を付している。

【0012】図1の(a)において、 $2R < L$ の場合に一対の櫛歯状電極の双方の電極指1a, 1bがショートすることはない。 $2R > L$ の場合には、微粒子12が複数の電極指上にわたって付着するが、IDT電極上(IDT電極上のみ)に保護膜13が設けられているのでショートすることはない。 $2R \approx L$ では、微粒子12が電極指1a, 1bの側面に接触してショートする可能性があるが、本実施形態では、 $H < L/2$ とされており、電極指1a, 1bの側面が微粒子12の最大幅の部分に達していない。従って、電極指1a, 1bの側面を通じてショートする確率が格段に小さくなる。

【0013】図1の(b)において、 $2R < L$ 及び $2R > L$ の場合には、(a)と同様にショートすることはない。本実施形態は、 $H \geq L/2$ のようにIDT電極の膜厚が比較的厚い場合に適用され、外部に露出している電極指1a, 1bの側面の高さ $H-P$ を $H-P < L/2$ とすることにより、電極指1a, 1bの側面が微粒子12の最大幅の部分に達していない。従って、電極指1a, 1bの側面を通じてショートする確率が格段に小さくなる。

【0014】上記保護膜13は電氣的に絶縁性又は半導電性(半導伝性)のものから成り、保護膜の抵抗率を $\rho$  ( $\Omega \cdot \text{cm}$ )としたとき、 $\rho/P$ が $10^9$  ( $\Omega$ )以上となるようにするのが好ましい。その材料としては、Ta, Mo及びそれらの酸化物若しくは窒化物、NiCr, NiCr-Si, Cr-SiO, Cr-SiO<sub>2</sub>, Si, SiO<sub>2</sub>, SiN等である。

【0015】本発明において、IDT電極はAlあるいはAl合金(Al-Cu系, Al-Ti系等)からなり、特にAlが励振効率が高く、材料コストが安価であり好ましい。また、電極形状は図1に示すような入出力用の櫛歯状電極(IDT電極)を交互に噛み合わせたような形状であるが、本発明は、複数の電極指を平行に配置した反射器のようなスリット型のものにも適用でき

る。更に、電極指1a, 1bの断面形状は、圧電基板面に向かって先細りとなるような逆テーパ型が、電極指1a, 1bの側面を通じてショートするのを抑制するうえで好ましい。

【0016】そして、IDT電極の対数は50~200程度、電極指1a, 1bの幅は0.1~10.0  $\mu\text{m}$ 程度、電極指1a, 1b間の間隔は0.1~10.0  $\mu\text{m}$ 程度、電極指1a, 1bの交差幅は10~80  $\mu\text{m}$ 程度、IDT電極の厚みは0.2~0.4  $\mu\text{m}$ 程度とすることが、共振器あるいはフィルタとしての所期の特性を得るうえで好適である。また、IDT電極のSAWの伝搬路の両端に、SAWを反射し効率良く共振させるための反射器を適宜設けてもよく、更には、電極指1a, 1b間にZnO, AlO等の圧電材料を成膜すれば、SAWの共振効率が向上し好適である。

【0017】上記圧電基板10としては、36° Yカット-X伝搬のLiTaO<sub>3</sub>結晶、64° Yカット-X伝搬のLiNbO<sub>3</sub>結晶、45° Xカット-Z伝搬のLiB<sub>3</sub>O<sub>6</sub>結晶、水晶等が好適であり、特に36° Yカット-X伝搬のLiTaO<sub>3</sub>結晶は通過帯域幅が広く、また45° Xカット-Z伝搬のLiB<sub>3</sub>O<sub>6</sub>結晶は電気機械結合係数が大きくかつ群遅延時間温度係数が小さいため好ましい。圧電基板10の厚みは0.3~0.5mmがよく、0.3mm未満では圧電基板10が脆くなり、0.5mm超ではコストが大きくなる。

【0018】かくして、本発明は、導電性の異物の付着による電極指間のショートを格段に抑制するという作用効果を有する。

【0019】更に、本発明のSAW装置は以下のように製造される。図1の(a)の場合、図3の工程に従う。まず、工程(a)で圧電基板10上にリフトオフ用の感光性レジストを塗布し、工程(b)でフォトリソグラフィによりIDT電極のネガパターンを形成する。その後、工程(c)で蒸着法、スパッタリング法、CVD法等の薄膜形成法により、真空雰囲気中でIDT電極用のAl等から成る導電膜を成膜する。そのとき、導電膜の膜厚が電極指1a, 1b間の間隔の $1/2$ 未満となるようにする。次に、工程(d)で真空を破らずに、IDT電極が形成された側の圧電基板表面に保護膜13を蒸着法等により成膜する。その膜厚は10~100nmが好適であり、10nm未満では絶縁性の保護膜13として機能するのに充分でなく、100nm超では共振器特性及びフィルタ特性に大きな影響を与える。そして、工程(e)でネガパターン部に相当する感光性レジスト、導電膜、保護膜13を同時にリフトオフし、本発明のSAW装置を得る。

【0020】図1の(b)の場合は以下の工程に従う。まず、圧電基板10上にリフトオフ用の感光性レジストを塗布し、フォトリソグラフィによりIDT電極のネガパターンを形成する。その後、蒸着法、スパッタリ

ング法、CVD法等の薄膜形成法により、Al等から成るIDT電極用の導電膜を成膜する。ネガパターンに相当する導電膜を、感光性レジストとともにリフトオフして除去しIDT電極を形成する。尚、IDT電極は、まず導電膜を形成して感光性レジストを塗布し、フォトリソグラフィ法によりIDT電極のポジパターンを形成した後、エッチング法によってポジパターンに相当する導電膜を残して形成してもかまわない。

【0021】次に、蒸着法、スパッタリング法、CVD法等の薄膜形成法により保護膜を形成する。その膜厚は、図1の(a)の場合と同様に10~100nmが好適である。このとき、IDT電極の膜厚と保護膜13の膜厚との差が、電極指1a、1b間の間隔の1/2未満になるようにし、本発明の弾性表面波装置を得る。

【0022】尚、本発明は上記の実施形態に限定されるものではなく、本発明の要旨を逸脱しない範囲内で種々の変更は何等差し支えない。

【0023】

【実施例】本発明の実施例を以下に示す。

【0024】(実施例1)図1の(a)に相当するSAW装置を以下のようにして作製した。36°Yカット-X伝搬のLiTaO<sub>3</sub>結晶から成る圧電基板10上に、リフトオフ用の感光性レジストを塗布し、フォトリソグラフィ法によりIDT電極のネガパターンを形成した。このとき、感光性レジストのベーク温度、ベーク時間、露光時の紫外線強度、露光時間、現像液、現像時間等の条件を調整して、感光性レジストをリフトオフしやすいようにその断面形状を逆テーパ形状とした。SAWをLiTaO<sub>3</sub>結晶のX軸方向に伝搬させるので、電極指1a、1bの長手方向はX軸方向に対して垂直になるようにした。また、約900MHz程度の信号を通過させるので、所望の特性を得るために、電極指1a、1bの幅が1.1μm、電極指1a、1b間の間隔が1.1μmとなるようにした。

【0025】次に、圧電基板10を真空蒸着機内に設置し、そのネガパターンが形成された側の圧電基板表面にAlを460nm成膜した。このとき、真空蒸着機のチャンパー内の真空度は10<sup>-7</sup>Torrとした。その後、真空を破らずに保護膜13用のSiを25nm成膜した。このとき、圧電基板10の焦電効果により電極指1a、1b間に放電が起こり、電極指1a、1bが損傷するのを避けるため、圧電基板10の加熱は行わなかった。そして、圧電基板10のネガパターンに相当する感光性レジスト、導電膜、保護膜13をリフトオフし、IDT電極及び保護膜13を形成し、SAW装置を作製した。

【0026】上記SAW装置は、(IDT電極の膜厚)=460nmで、一方、(電極指1a、1b間の間隔の1/2)=1.1(μm)/2=550(nm)であった。前記構成とすることにより、従来不良率が数%であ

ったものが、0.1%程度に減少した。また、従来に比較して真空引きが1回で済むため、その分SAW装置を低コストに製造できた。

【0027】(実施例2)図1の(b)に相当するSAW装置を以下のようにして作製した。36°Yカット-X伝搬のLiTaO<sub>3</sub>結晶から成る圧電基板10上に、リフトオフ用の感光性レジストを塗布し、フォトリソグラフィ法によりIDT電極のネガパターンを形成した。このとき、感光性レジストのベーク温度、ベーク時間、露光時の紫外線強度、露光時間、現像液、現像時間等の条件を調整して、リフトオフしやすいようにその断面形状を逆テーパ形状とした。SAWをLiTaO<sub>3</sub>結晶のX軸方向に伝搬させるので、電極指1a、1bの長手方向はX軸方向に対して垂直になるようにした。また、約900MHz程度の信号を通過させるので、所望の特性を得るために、電極指1a、1bの幅が1.1μm、電極指1a、1b間の間隔が1.1μmとなるようにした。

【0028】次に、圧電基板10を真空蒸着機内に設置し、そのネガパターンが形成された側の圧電基板表面にAlを460nm成膜した。このとき、真空蒸着機のチャンパー内の真空度は10<sup>-7</sup>Torrとした。蒸着後の圧電基板10のネガパターンに相当する感光性レジストをリフトオフし、IDT電極を形成した。その後、圧電基板10を真空蒸着機内に設置し、10<sup>-7</sup>Torr台まで真空引きし、保護膜13用のSiを25nm成膜してSAW装置を作製した。このとき、圧電基板10の焦電効果により電極指間に放電が起こり、電極指が損傷するのを避けるため、圧電基板10の加熱は行わなかった。

【0029】上記SAW装置は、(IDT電極の膜厚)-(保護膜13の膜厚)=460-25=435(nm)で、一方、(電極指1a、1b間の間隔の1/2)=1.1(μm)/2=550(nm)であるので、IDT電極の膜厚と保護膜13の膜厚の差435nmが、電極指1a、1b間の間隔の1/2の550nmよりも小さい値となっている。前記構成にすることにより、実施例1と同様の効果が得られた。

【0030】

【発明の効果】本発明の第1の発明は、櫛歯状電極上のみに保護膜が設けられ、櫛歯状電極の膜厚を電極指間の間隔の1/2未満とすることにより、パッケージング等の組み立て加工時に導電性の異物が付着して電極指間にショートが発生するのを格段に抑制できるという効果を奏する。また、真空を破らずに櫛歯状電極と保護膜を連続で成膜でき、フォトリソグラフィ工程も1回で済むので、工程が簡略化される。更に、真空を解放するとき外部から雰囲気中に異物が混入して付着する等の汚染が低減する。櫛歯状電極を形成し終わる前に保護膜を成膜するので、保護膜形成時の焦電効果による電極指間の放電がなく、電極指が損傷しないという効果も有する。

(5)

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【0031】また、第2の発明は、櫛歯状電極及び圧電基板表面に保護膜が設けられ、櫛歯状電極の膜厚と保護膜の膜厚との差を電極指間の間隔の1/2未満とすることにより、上記と同様に電極指間にショートが発生するのを格段に抑制できる。この場合、電極指の側面に保護膜を被覆する必要はなく、あるいは何らかの原因により電極指の側面に保護膜が被覆されなかったとき、本発明のように櫛歯状電極の膜厚を調整しておけばショートを抑制することができる。従って、被覆性の悪い成膜装置、成膜方法でも成膜できるので、成膜設備に制約されず低コストで製造可能となる。成膜のしにくい電極指の側面の被覆を必要としないので、保護膜の膜厚を薄くでき、成膜のタクトタイムが短くなり生産性がよい。また、保護膜の薄膜化により共振器特性及びSAWフィルタ特性への影響を小さくでき、故に設計の自由度が向上する。

【0032】更に、本発明は、導電性の異物がある程度付着してもショートする確率がかなり小さいため、導電性の異物の主な発生源であるパッケージを余分に洗浄す\*

る必要がなくなり、その結果、製造工程が簡略化できる。

【図面の簡単な説明】

【図1】本発明のSAW装置を示し、(a)はIDT電極上のみ保護膜があるものの部分拡大断面図、(b)は全面に保護膜があるものの部分拡大断面図である。

【図2】従来のSAW装置を示し、(a)は保護膜がないものの部分拡大断面図、(b)は全面に保護膜があるものの部分拡大断面図である。

【図3】本発明のSAW装置の製造工程の流れ図で、(a)～(e)は各工程の内容を示す。

【図4】従来のSAW装置の製造工程の流れ図で、(a)～(e)は各工程の内容を示す。

【符号の説明】

1a：電極指

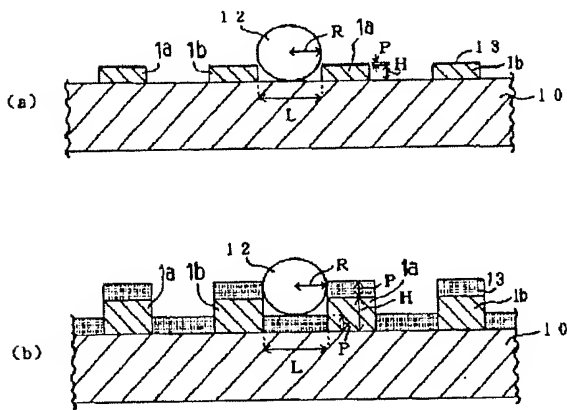
1b：電極指

10：圧電基板

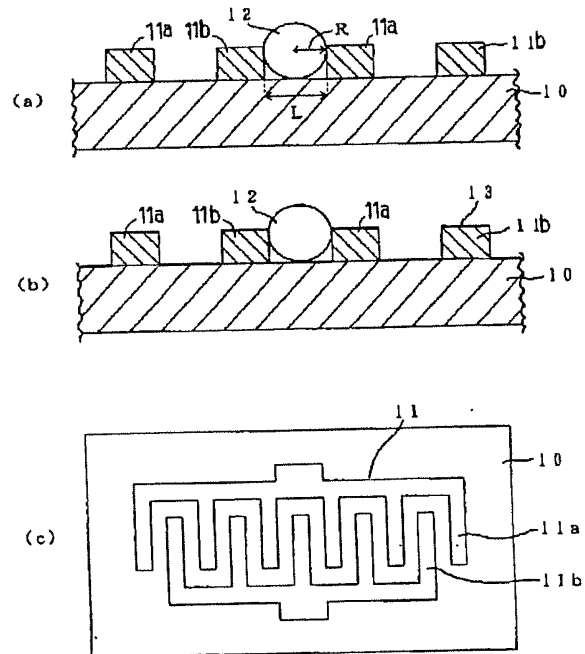
12：導電性の微粒子

13：保護膜

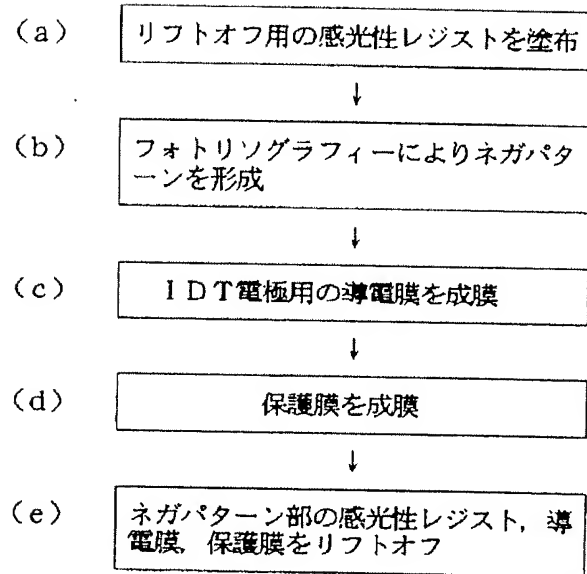
【図1】



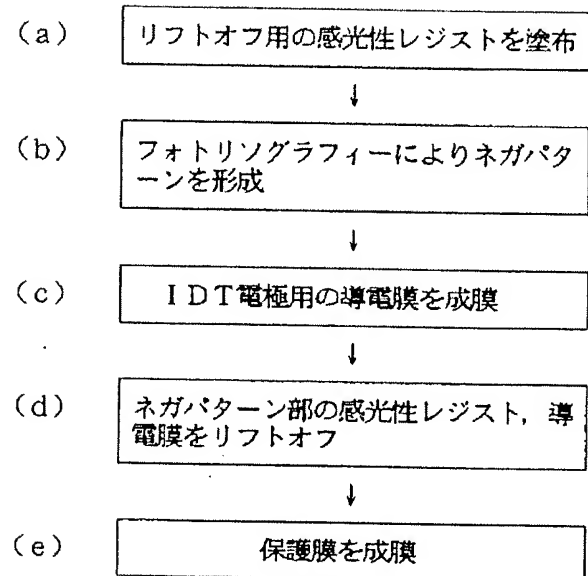
【図2】



【図3】



【図4】



## 【手続補正書】

【提出日】平成8年12月10日

## 【手続補正1】

【補正対象書類名】明細書

【補正対象項目名】図2

【補正方法】変更

## \* 【補正内容】

【図2】従来のSAW装置を示し、(a)は保護膜がないものの部分拡大断面図、(b)は全面に保護膜があるものの部分拡大断面図、(c)はSAW装置全体の基本構成の平面図である。

\*

フロントページの続き

(72)発明者 加賀井 恵美  
京都府相楽郡精華町光台3丁目5番地 京セラ株式会社中央研究所内

(72)発明者 旗手 淳雄  
京都府相楽郡精華町光台3丁目5番地 京セラ株式会社中央研究所内